Haga Property – Lot 2 2107 Bayfield Parkway, Bayfield, CO Drainage Narrative September 14, 2023 By: PST Engineering LLC



## **Background**

The Haga Property is a 17-acre parcel located south of US Highway 160, north and west of Bayfield Parkway, and east of the Church of Christ of Bayfield. The entire Haga Property is being subdivided into future commercial and residential lots as part of the Master Plan. PST Engineering prepared the *Haga Property – Master Plan Drainage Study (Master Study)* dated March 10, 2023 which describes the proposed drainage conditions of the overall property.

Lot 2 is the proposed lot south of Road E-W and west of Road N-S. The purpose of this study is to analyze the drainage conditions internal to Lot 2 and validate the assumptions made about Lot 2 in the *Master Study*.

## **Existing Conditions**

Lot 2 is currently irrigated grazing land west of the Schroder Ditch and east of the existing residence that will remain in Lot 1. The site generally surface flows from southeast to northwest to a ditch on the west property line and into an existing 18-in CMP culvert (the design point analyzed in the *Master Study*.)

As described in the *Master Study*, soils for the site were found to be classified as Hydrological Soil Group D. Onsite soils are all Corta loam, with 1 to 3 percent slopes described as well drained with medium runoff.

## **Proposed Conditions**

Lot 2 is proposed to be the first development to be constructed in the overall Haga development. As such, Road N-S is proposed to be installed to the Lot 2 entrance. The irrigation ditch will also be piped as part of the initial construction which will require the installation of Culverts A & B and Ditch C, all described in the *Master Study*. Road E-W and Road N-S outside of the hardscape improvements will be graded to subgrade as part of the initial construction. The overall Haga pond in Tract A will also be constructed in its entirety.

In addition to the Master Plan improvements, Lot 2 will see the construction of a private street, 33 multi-family residential units, an off-street parking lot, improvements to Bayfield Parkway and a series of storm drainage conveyance features including a private storm drain line.

## **Detention**

Detention was designed to be provided for Lot 2 by the pond in Tract A that was designed to provide flow attenuation for the overall Haga development. Calculations for the pond assumed a land cover for

### Haga Property – Lot 2 2107 Bayfield Parkway, Bayfield, CO Drainage Narrative September 14, 2023 By: PST Engineering LLC



Lot 2 in the *Master Study*. The land cover assumption was found to be conservative as the composite curve number for the proposed development was found to be less than what was assumed, as summarized in Table 1.

Table 1: Assumed	vs. Proposed	Land Cover fo	or Lot 2

Description	Area (acres)	Curve Number
Proposed Open Space – Good Condition	1.81	80
Proposed Impervious Area	1.31	98
Composite Curve Number	3.12	88
Assumed in Master Study	3.12	92

See Appendix A for an exhibit showing the proposed land cover of Lot 2.

#### **Conveyance**

Proposed conveyance features include curb, gutter, inlets, storm drain pipe and ditches to convey flow to the detention pond. *Hydraflow Express Extension for Autodesk Civil3D* (*Express*) was used to model the capacity of the inlets, culverts and ditches, as well as to model curb & gutter spread at the proposed inlets. Conveyance features are discussed in more detail in the following subsections.

The rational method was used to calculate flows to each of the analyzed features. Per Section 5.2.2.B of the *Town of Bayfield Infrastructure Design Standards* (*Design Standards*)– the minimum time of concentration used was 10-minutes. Rainfall intensities were taken from NOAA Atlas 14, Volume 8, Version 2 which were found to be more conservative than the values in Table 5.2 of the *Design Standards*. Rainfall data can be found in Appendix H.

See Appendix B for a map delineating sub-basins for each drainage feature and Appendix C for rational method calculation results.

#### <u>Inlets</u>

The low point of the Lot 2 private road was designed to be drained by Inlets Y1 & Inlets Y2. Inlets Y1 & Y2 were designed as Town of Bayfield standard single inlets with combination grates in a sag condition. Inlets Y1 & Y2 were modelled in *Express* with a 50% clogging factor. *Express* modelling shows that curb overtopping is not expected during the 100-year storm event.

Inlet Y3 was designed as a 24-in area drain with beehive grate to drain a swale near the amenity area. This inlet was design using the *Nyoplast Dome Grate Inlet Capacity Chart* for 6.04-cfs – double the Q100 calculated in Appendix C to model a 50% clogging factor. The head required to convey this flow is not expected to back up to overtop sidewalks or reach any adjacent building foundations.

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See Appendix K for *Express* output and Nyoplast Capacity Charts.

#### Storm Drain

Storm drain pipe from the inlets described in the previous section were all designed using the *Hydraflow Storm Sewer Extension for Autodesk Civil3D* (*Storm Sewer*) to keep the hydraulic grade line below finish grade for the major storm events.

See Appendix E for *Storm Sewer* Output

#### **Culvert**

A culvert was designed as part of Lot 2 to convey flow beneath the proposed emergency access road. Culvert 1 (18-in) was designed to convey flow from the swale south of the southern-most townhome units to the Tract A pond.

Flows the culvert subbasin were calculated in Appendix C and *Express* was used to model both culverts in the major storm event.

See Appendix F for *Express* output.

#### <u>Swales</u>

Several swales were designed to convey flow from Lot 2. *Express* was used to model the swales based on the proposed geometry and flows from Appendix C and show no overtopping.

See Appendix G for Express output

## Haga Property – Lot 2 2107 Bayfield Parkway, Bayfield, CO Drainage Narrative



September 14, 2023 By: PST Engineering LLC

#### LIST OF APPENDICES

- Appendix A: Land Cover Analysis
- Appendix B: Drainage Feature Sub-Basins
- Appendix C: Rational Method Flow Results
- Appendix D: Inlet Analysis
- Appendix E: Storm Drain Analysis
- Appendix F: Culvert Analysis
- Appendix G: Swale Analysis
- Appendix H: Rainfall Data from NOAA Atlas 14, Volume 8, Version 2



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## APPENDIX C: LOT 2 SUB-BASIN FLOW CALCULATIONS

#### LOT 2 SUB-BASIN FLOW CALCULATIONS

1	2	3	4	5	6	7		7 8		9	
Basin ID	Impervious Area (Acres)	Open Space Area (Acres)	Total Area (Acres)	Impervious Percentage	Time of Concentration (Minutes)	5-Year Rainfall Intensity (in/hr)	100-Year Rainfall Intensity (in/hr)	5-Year Runoff Coefficient	100-Year Runoff Coefficient	5-Year Flow (cfs)	100-Year Flow (cfs)
Inlet Y1	0.6	0.25	0.85	71%	10	2.75	6.76	0.614	0.773	1.43	4.44
Inlet Y2	0.73	0.22	0.95	77%	10	2.75	6.76	0.665	0.799	1.74	5.13
Inlet Y3	0.25	0.46	0.71	35%	10	2.75	6.76	0.324	0.628	0.63	3.02
Culvert 1	0.2	0.71	0.91	22%	10	2.75	6.76	0.215	0.574	0.54	3.53

Notes:

1. See Basin Map Appendix B

2. As Measured in CAD

3. As Measured in CAD

4. Column 2 + Column 3

5. Column 2 / Column 4

6. 10 Minutes = Town of Bayfield minimum per Section 5.2.2.B of the Infrastructure Design Guide

7. From NOAA Atlas 14, Volume 8, Version 2

8. From Table 6-4 of the *Urban Storm Drainage Criteria Manual Volume 1* - for Type D Soils

9. Q = C\*I\*A

SEE BELOW

TABLE 6-4 INCLUDED BELOW FOR "C" VALUE CALCULATIONS

#### Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

NRCS			Storm Return Period							
Soil Group	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year			
Α	C <sub>A</sub> =	C <sub>A</sub> =	C <sub>A</sub> =	C <sub>A</sub> =	C <sub>A</sub> =	C <sub>A</sub> =	C <sub>A</sub> =			
	0.84 <i>i</i> <sup>1.302</sup>	0.86 <i>i</i> <sup>1.276</sup>	$0.87i^{1.232}$	$0.88i^{1.124}$	0.85 <i>i</i> +0.025	0.78 <i>i</i> +0.110	0.65 <i>i</i> +0.254			
В	$C_B =$	$C_B =$	$C_B =$	$C_B =$	$C_B =$	$C_B =$	$C_B =$			
	0.84 <i>i</i> <sup>1.169</sup>	$0.86i^{1.088}$	0.81 <i>i</i> +0.057	0.63 <i>i</i> +0.249	0.56 <i>i</i> +0.328	0.47 <i>i</i> +0.426	0.37 <i>i</i> +0.536			
C/D	C <sub>C/D</sub> =	C <sub>C/D</sub> =	C <sub>C/D</sub> =	C <sub>C/D</sub> =	C <sub>C/D</sub> =	C <sub>C/D</sub> =	C <sub>C/D</sub> =			
	$0.83i^{1.122}$	0.82 <i>i</i> +0.035	0.74 <i>i</i> +0.132	0.56 <i>i</i> +0.319	0.49 <i>i</i> +0.393	0.41 <i>i</i> +0.484	0.32 <i>i</i> +0.588			

# **Inlet Report**

## APPENDIX D-1: INLET Y1 ANALYSIS

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

## **INLET Y1**



Monday, Mar 6 2023

# **Inlet Report**

## **APPENDIX D-2: INLET Y2 ANALYSIS**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

## **INLET Y2**



Monday, Mar 6 2023

APPENDIX D-3: INLET Y3 ANALYSIS

Nyloplast 24" Dome Grate Inlet Capacity Chart





3130 Verona Avenue • Buford, GA 30518 (866) 888-8479 / (770) 932-2443 • Fax: (770) 932-2490 © Nyloplast Inlet Capacity Charts June 2012

## **Storm Sewer Profile**



#### **APPENDIX E-2: STORM SEWER HGL REPORT Storm Sewer Summary Report** Flow Line Line HGL HGL HGL Line Line ID Line Invert Line Minor Dns Junction Invert No. Size shape length EL Dn EL Up Slope Down Up Junct Line rate loss Type (ft) (ft) (cfs) (in) (ft) (ft) (%) (ft) (ft) (ft) No. 0.21 Y1 12.59 18 Cir 74.434 6973.40 6973.77 0.497 6974.74\* 6975.70\* 6975.91 End Manhole 1 2 Y2 8.15 18 Cir 44.023 6973.97 6974.19 0.499 6975.91\* 6976.14\* 0.31 6976.45 1 Manhole 6976.84\* 0.23 3 Y3 2 3.02 12 Cir 64.080 6974.69 6975.33 0.999 6976.45\* 6977.07 Manhole $\Lambda$ HGL ABOVE PIPE CROWN, BUT BELOW FINISH GRADE IN ALL CASES FROM APPENDIX C -UPSTREAM LINES ADDED Project File: Storm Y.stm Number of lines: 3 Run Date: 3/6/2023 NOTES: Known Qs only ; \*Surcharged (HGL above crown).

Page 1

# **Culvert Report**

# **APPENDIX F-1: CULVERT 1 ANALYSIS**

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Sep 11 2023

## **CULVERT 1**

Invert Elev Dn (ft)	= 6976.00		Calculations	
Pipe Length (ft)	= 43.00		Qmin (cfs)	= 3.53
Slope (%)	= 3.67		Qmax (cfs)	= 3,53
Invert Elev Up (ft)	= 6977.58		Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 18.0			
Shape	= Circular		Highlighted	
Span (in)	= 18.0		Qtotal (cfs)	= 3.53
No. Barrels	= 1		Qpipe (cfs)	= 3.53
n-Value	= 0.011		Qovertop (cfs)	= 0.00
Culvert Type	= Circular C	ulvert	Veloc Dn (ft/s)	= 2.52
Culvert Entrance	= Smooth ta	pered inlet throat	Veloc Up (ft/s)	= 4.24
Coeff. K,M,c,Y,k	= 0.534, 0.5	55, 0.0196, 0.9, 0.2	HGL Dn (ft)	= 6977.11
			HGL Up (ft)	= 6978.30
Embankment			Hw Elev (ft)	= 6978.63
Top Elevation (ft)	= 6981.00		Hw/D (ft)	= 0.70
Top Width (ft)	= 12.00		Flow Regime	= Inlet Control
Crest Width (ft)	= 30.00		Ŭ	
				JRING 100-YEAR STORM
6982.00	r	CULVERT	ii	4.42
6981.00				3.42
6980.00				2.42
6979.00				1.42
				-inlet control
6978.00	1			0.42
6977.00				-0.58
6976.00				-1.58
6975.00 0 5	10 15 20	25 30 35 40	D 45 50 55	60 65 -2.58
Circular Culve	rt HGL	Embank		Reach (ft)

# **Channel Report**

**APPENDIX G-1: INLET Y3 SWALE** 

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Mar 6 2023

## DITCH TO INLET Y3

Triangular		Highlighted	
Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 0.72
Total Depth (ft)	= 1.00	Q (cfs)	= 3.020
		🕂 Area (sqft)	= 1.56
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 1.94
Slope (%)	= 0.50	/ Wetted Perim (ft)	= 4.55
N-Value	= 0.026	Crit Depth, Yc (ft)	= 0.58
		Top Width (ft)	= 4.32
Calculations		EGL (ft)	= 0.78
Compute by:	Known Q		
Known Q (cfs)	= 3.02		
		_ /	
	INLET Y3 BASIN Q100		



Reach (ft)

# **Channel Report**

**APPENDIX G-2: SWALE TO CULVERT 1** 

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Sep 11 2023

## Swale to Culvert 1

Triangular		Highlighted	
Side Slopes (z:1)	= 3.00, 3.00	Depth (ft)	= 0.76
Total Depth (ft)	= 1.00	Q (cfs)	= 3.530
		🕂 Area (sqft)	= 1.73
Invert Elev (ft)	= 1.00	Velocity (ft/s)	= 2.04
Slope (%)	= 0.50	/ Wetted Perim (ft)	= 4.81
N-Value	= 0.026	Crit Depth, Yc (ft)	= 0.62
		Top Width (ft)	= 4.56
Calculations		EGL (ft)	= 0.82
Compute by:	Known Q		
Known Q (cfs)	= 3.53		
		_ /	
	CULVERT 1 BASIN Q100	$\vdash$	



Reach (ft)

APPENDIX H: RAINFALL DATA

Precipitation Frequency Data Server



NOAA Atlas 14, Volume 8, Version 2 Location name: Bayfield, Colorado, USA\* Latitude: 37.2317°, Longitude: -107.5912° Elevation: m/ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF\_tabular | PF\_graphical | Maps\_&\_aerials

#### PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) <sup>1</sup>										
Duration				Avera	ge recurren	ce interval (	years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>2.21</b> (1.74-2.87)	<b>2.74</b> (2.15-3.55)	<b>3.76</b> (2.95-4.90)	<b>4.75</b> (3.71-6.20)	<b>6.32</b> (4.87-8.76)	<b>7.70</b> (5.75-10.7)	<b>9.23</b> (6.65-13.0)	<b>10.9</b> (7.56-15.7)	<b>13.4</b> (8.90-19.6)	<b>15.4</b> (9.92-22.6)
10-min	<b>1.61</b>	<b>2.00</b>	<mark>2.75</mark>	<b>3.47</b>	<b>4.63</b>	<b>5.64</b>	<mark>6.76</mark>	<b>7.99</b>	<b>9.80</b>	<b>11.3</b>
	(1.27-2.09)	(1.58-2.60)	(2.16-3.59)	(2.71-4.55)	(3.56-6.41)	(4.21-7.82)	(4.87-9.53)	(5.53-11.5)	(6.52-14.4)	(7.27-16.5)
15-min	<b>1.31</b>	<b>1.63</b>	<b>2.24</b>	<b>2.83</b>	<b>3.76</b>	<b>4.58</b>	<b>5.49</b>	<b>6.50</b>	<b>7.97</b>	<b>9.18</b>
	(1.03-1.70)	(1.28-2.12)	(1.75-2.92)	(2.20-3.70)	(2.90-5.21)	(3.42-6.36)	(3.96-7.75)	(4.50-9.34)	(5.30-11.7)	(5.91-13.4)
30-min	<b>0.818</b>	<b>1.04</b>	<b>1.45</b>	<b>1.84</b>	<b>2.44</b>	<b>2.96</b>	<b>3.52</b>	<b>4.14</b>	<b>5.02</b>	<b>5.75</b>
	(0.644-1.06)	(0.820-1.35)	(1.14-1.89)	(1.44-2.41)	(1.87-3.36)	(2.20-4.09)	(2.53-4.95)	(2.86-5.93)	(3.34-7.34)	(3.70-8.41)
60-min	<b>0.459</b>	<b>0.627</b>	<b>0.914</b>	<b>1.16</b>	<b>1.52</b>	<b>1.81</b>	<b>2.12</b>	<b>2.43</b>	<b>2.87</b>	<b>3.22</b>
	(0.362-0.597)	(0.493-0.816)	(0.716-1.19)	(0.906-1.52)	(1.15-2.07)	(1.34-2.48)	(1.51-2.95)	(1.67-3.46)	(1.90-4.17)	(2.07-4.71)
2-hr	<b>0.255</b>	<b>0.367</b>	<b>0.550</b>	<b>0.702</b>	<b>0.912</b>	<b>1.07</b>	<b>1.24</b>	<b>1.40</b>	<b>1.62</b>	<b>1.78</b>
	(0.203-0.326)	(0.292-0.470)	(0.437-0.706)	(0.554-0.904)	(0.694-1.21)	(0.800-1.43)	(0.892-1.68)	(0.971-1.95)	(1.08-2.30)	(1.16-2.57)
3-hr	<b>0.185</b>	<b>0.268</b>	<b>0.402</b>	<b>0.510</b>	<b>0.656</b>	<b>0.765</b>	<b>0.871</b>	<b>0.976</b>	<b>1.11</b>	<b>1.21</b>
	(0.149-0.235)	(0.215-0.341)	(0.322-0.511)	(0.406-0.652)	(0.501-0.855)	(0.573-1.01)	(0.632-1.17)	(0.682-1.34)	(0.748-1.56)	(0.799-1.73)
6-hr	<b>0.125</b>	<b>0.163</b>	<b>0.226</b>	<b>0.277</b>	<b>0.347</b>	<b>0.400</b>	<b>0.453</b>	<b>0.505</b>	<b>0.574</b>	<b>0.626</b>
	(0.101-0.156)	(0.133-0.204)	(0.183-0.283)	(0.223-0.348)	(0.270-0.446)	(0.304-0.520)	(0.334-0.600)	(0.359-0.684)	(0.393-0.795)	(0.420-0.879)
12-hr	<b>0.086</b>	<b>0.102</b>	<b>0.128</b>	<b>0.150</b>	<b>0.182</b>	<b>0.207</b>	<b>0.232</b>	<b>0.258</b>	<b>0.293</b>	<b>0.321</b>
	(0.071-0.106)	(0.084-0.125)	(0.105-0.158)	(0.123-0.186)	(0.144-0.231)	(0.160-0.265)	(0.174-0.304)	(0.187-0.345)	(0.205-0.401)	(0.218-0.443)
24-hr	<b>0.056</b>	<b>0.063</b>	<b>0.075</b>	<b>0.085</b>	<b>0.100</b>	<b>0.112</b>	<b>0.125</b>	<b>0.138</b>	<b>0.157</b>	<b>0.171</b>
	(0.047-0.068)	(0.053-0.077)	(0.062-0.091)	(0.071-0.104)	(0.081-0.126)	(0.089-0.142)	(0.096-0.161)	(0.102-0.182)	(0.111-0.211)	(0.119-0.233)
2-day	<b>0.034</b>	<b>0.038</b>	<b>0.046</b>	<b>0.052</b>	<b>0.061</b>	<b>0.068</b>	<b>0.074</b>	<b>0.081</b>	<b>0.090</b>	<b>0.097</b>
	(0.028-0.040)	(0.032-0.046)	(0.039-0.055)	(0.044-0.063)	(0.050-0.075)	(0.054-0.084)	(0.058-0.094)	(0.061-0.105)	(0.065-0.119)	(0.068-0.130)
3-day	<b>0.025</b>	<b>0.028</b>	<b>0.034</b>	<b>0.039</b>	<b>0.045</b>	<b>0.050</b>	<b>0.055</b>	<b>0.060</b>	<b>0.066</b>	<b>0.071</b>
	(0.021-0.030)	(0.024-0.034)	(0.029-0.040)	(0.033-0.046)	(0.037-0.055)	(0.040-0.061)	(0.043-0.069)	(0.045-0.076)	(0.048-0.086)	(0.051-0.094)
4-day	<b>0.020</b>	<b>0.023</b>	<b>0.028</b>	<b>0.031</b>	<b>0.036</b>	<b>0.040</b>	<b>0.044</b>	<b>0.048</b>	<b>0.053</b>	<b>0.057</b>
	(0.017-0.024)	(0.020-0.027)	(0.024-0.032)	(0.027-0.037)	(0.030-0.044)	(0.033-0.049)	(0.035-0.055)	(0.036-0.061)	(0.039-0.069)	(0.041-0.075)
7-day	<b>0.014</b>	<b>0.016</b>	<b>0.018</b>	<b>0.021</b>	<b>0.024</b>	<b>0.027</b>	<b>0.029</b>	<b>0.032</b>	<b>0.036</b>	<b>0.038</b>
	(0.012-0.016)	(0.013-0.018)	(0.016-0.021)	(0.018-0.024)	(0.020-0.029)	(0.022-0.032)	(0.023-0.036)	(0.025-0.040)	(0.026-0.045)	(0.028-0.049)
10-day	<b>0.011</b>	<b>0.012</b>	<b>0.014</b>	<b>0.016</b>	<b>0.019</b>	<b>0.021</b>	<b>0.023</b>	<b>0.025</b>	<b>0.027</b>	<b>0.029</b>
	(0.009-0.012)	(0.011-0.014)	(0.013-0.017)	(0.014-0.019)	(0.016-0.022)	(0.017-0.025)	(0.018-0.028)	(0.019-0.031)	(0.021-0.035)	(0.022-0.038)
20-day	<b>0.007</b>	<b>0.008</b>	<b>0.009</b>	<b>0.010</b>	<b>0.012</b>	<b>0.013</b>	<b>0.014</b>	<b>0.015</b>	<b>0.017</b>	<b>0.018</b>
	(0.006-0.008)	(0.007-0.009)	(0.008-0.011)	(0.009-0.012)	(0.010-0.014)	(0.011-0.015)	(0.011-0.017)	(0.012-0.019)	(0.013-0.021)	(0.013-0.022)
30-day	<b>0.006</b>	0.006	<b>0.007</b>	<b>0.008</b>	0.009	0.010	<b>0.011</b>	0.012	<b>0.013</b>	<b>0.014</b>
	(0.005-0.006)	(0.006-0.007)	(0.007-0.008)	(0.007-0.009)	(0.008-0.011)	(0.009-0.012)	(0.009-0.013)	(0.009-0.014)	(0.010-0.016)	(0.010-0.017)
45-day	0.005	0.005	<b>0.006</b>	<b>0.007</b>	0.008	0.008	0.009	0.010	0.010	<b>0.011</b>
	(0.004-0.005)	(0.005-0.006)	(0.005-0.007)	(0.006-0.007)	(0.007-0.009)	(0.007-0.009)	(0.007-0.010)	(0.008-0.011)	(0.008-0.013)	(0.008-0.014)
60-day	<b>0.004</b>	<b>0.004</b>	<b>0.005</b>	<b>0.006</b>	<b>0.007</b>	<b>0.007</b>	<b>0.008</b>	<b>0.008</b>	<b>0.009</b>	<b>0.010</b>
	(0.004-0.004)	(0.004-0.005)	(0.005-0.006)	(0.005-0.006)	(0.006-0.007)	(0.006-0.008)	(0.006-0.009)	(0.007-0.010)	(0.007-0.011)	(0.007-0.012)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**PF graphical**